Mostafa

Design and Performance of the DSS

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ABSTRACT

Emerge Digital Sensor System (DSS) is a fully integrated fully digital ruggedized system for airborne image acquisition and georeferencing. The DSS consists of a 4K x 4K digital camera, POS/AV direct georeferencing system, and a flight management system. The DSS digital camera component uses a CCD chip with a 9 µm pixel size which allows digital image acquisition with a Ground Sample Distance that ranges from 0.15 m to 1.0 m using its 35 mm and 55 mm lenses. The DSS is used primarily to generate high-resolution color and color infrared digital orthophotos and orthomosaics. The DSS data interfaces directly and seamlessly with commercial off-the-shelf photogrammetric software to allow for fast map production. Orthophotos are created using the DSS-derived directly georeferenced digital images and a Digital Elevation Model (DEM). The orthophotos and/or orthomosaics can then be used for many different mapping, GIS and remote sensing applications. Examples of these are updating and maintaining cadastral GIS databases, classifying and mapping pervious and impervious surface areas, identifying wetland areas, updating land use maps, estimating crop yields and health, preparing timber stand inventories, planning for new construction sites, verifying areas for licensing and permitting. Many of these applications involve small localized areas, corridors, or irregular spot shots, which make the medium format DSS the suitable tool to complete the job. In this paper, an overview of the system design, calibration, and performance is presented in some detail.

1. INTRODUCTION

During the past two decades, the mapping sciences have progressively moved towards digital mapping, making use of multi disciplinary developments in the geomatics field. Instead of regarding geodesy, photogrammetry, and remote sensing as separate sciences, they are seen more as an integrated discipline today. Part of this development has been spurred on by systems capable of acquiring and fusing accurate globally referenced data in fully digital form with short turn around time in a cost effective fashion. A multi sensor system is, thus, the product of integrating the concepts of kinematic geodesy, aerospace engineering, automatic control, remote sensing, and digital photogrammetry, to acquire, store, and process measurable quantities that sufficiently describe spatial and/or physical characteristics of a part of the Earth's surface.

Emerge Digital Sensor System (DSS) is designed based on the concept of multidisciplinary developments. The DSS is a fully operational, fully integrated, and fully digital multi-sensor system developed for digital mapping data acquisition. The DSS consists of a 4K x 4K digital camera, POS/AV direct georeferencing system, and a flight management system. Figure 1 shows the components of the DSS. The DSS is used primarily to generate high-resolution colour and colour infrared digital orthophotos and orthomosaics using direct georeferencing techniques. The orthophotos are created using the POS AV direct exterior orientation data and a Digital Elevation Model (DEM). The orthophotos and/or orthomosaics can then be used for many different mapping, GIS and remote sensing applications. Examples of these are:

- 1. Updating and maintaining cadastral GIS databases
- 2. Classifying and mapping pervious and impervious surface areas
- 3. Identifying wetland areas
- 4. Update land use maps
- 5. Estimate crop yields and health
- 6. Prepare timber stand inventories
- 7. Plan for new constructions sites
- 8. Verify areas for licensing and permitting

Many of these applications involve small localized areas, corridors, or irregular spot shots, which make the medium format DSS the ideal tool to complete the job. With its small size, light weight, and low power consumption, the DSS is easy to install in light aircrafts or helicopters. Furthermore, it can be configured for pilot-only operation.

The Ground Sample Distance (GSD) or ground resolution achievable by the DSS ranges from 0.15 m to 1.0 m. The DSS uses modified off-the-shelf components. One of the main advantages of that approach is that, there is a clear upgrade path when new CCD technology is introduced into the commercial market place. For example, the DSS will have an upgrade path to the new larger CCD's (such as $4K \times 5K$) when they become available, and its modularity means it can be used together with a second camera to produce a DualCam for increased coverage.

a) DSS Control Unit



b) DSS Digital Imager c)

c) Flight Management System





Figure 1: Emerge DSS Components

The DSS imager has been modified to accommodate the aerial survey requirements, such as:

- Each digital back is custom machined to remove the effects of tilts and bowing in the CCD
- The camera body is modified to allow the digital back to be rigidly attached to the camera
- The CCD's are high grade quality and are cherry picked for minimum flaws
- The lenses use a special locking mechanism and are optimized for focus at infinity
- The digital back is modified to allow it to do both color and CIR imaging
- The camera is mounted in a proprietary exoskeleton (patent pending) designed to keep the lens, the camera body, and the IMU rigid with respect to each other
- The CCD is calibrated to remove effects of flaws
- The system has been ruggedized to survive the shock and vibrations exposed to in the airborne mapping environment.

2. THE DSS DATA FLOW

Figure 2 depicts the top-level procedure for data flow, where the POS AV data is run through POSPAC software, while the image data is run through Emerge ImageView Software. The radiometrically calibrated images together with their Exterior Orientation parameters are then imported into commercial third-party Automatic Tiepoint Generation (ATG) software to generate a number of tie/pass points per each image. Then, the image coordinates of tie/pass/GCP, the exterior orientation parameters, and any other available information are imported in POSCalTM software to calibrate the camera/IMU boresight and to do quality control of the camera calibration parameters and datum definition. Then, the data is looped once or twice between the ATG and POSCalTM softwares to obtain the ideal solution for the aforementioned calibration parameters. Then, as a final quality control step, the QC'd exterior orientation parameters, camera calibration parameters, and datum shifts (if any) are imported in a digital photogrammetric workstation to check the DSS-computed GCP ground coordinates against the land-surveyed ones, and to check the remaining y-parallax.

3. THE DSS CALIBRATION

The DSS is calibrated radiometrically using MacBeth targets, integrating spheres, and optimization software. Focus is set using conjugate white noise and MTF. Pixel and column defects are calibrated and removed through interpolation. Dark signal and pixel level gain corrections are also calibrated.

The DSS is calibrated geometrically using two methods: a terrestrial calibration followed by an airborne calibration. In the terrestrial calibration the interior orientation (focal length, lens distortions, principle point) and the IMU/camera boresight angles are measured using a calibration cage that is imaged from several angles. Then, the first time the system is installed in an aircraft, a boresight range is flown, and the POSCALTM software is used to refine the calibration parameters.



Figure 2: The DSS Data Flow



Figure 3: The DSS Calibration Cage

4. THE DSS PERFORMANCE ANALYSIS

This Section is dedicated to highlight the performance of The DSS. A number of test flights have been flown especially for that purpose. The results from one of the test flights are presented herein as an example. In December 2002, a test flight has been flown over a test field in Lakeland, Florida, USA. The objective of this flight was for testing and validation of the DSS calibration using aerial data as well as to analyse the performance of the DSS system in its entirety. A total of 65 images were collected in this flight from about 2000 m flight altitude Above Ground Level (AGL). A total of 33 Ground Control Points (GCPs) were land-surveyed using GPS by Emerge and NOAA Remote Sensing division. The flight trajectory is shown in Figure 4. The POS AV data was first processed using POSPAC. Figure 5 shows the estimated precision of the exposure station coordinates using airborne GPS data, processed in differential mode. A number of Continuously Operating Reference Stations (CORS) were used in the producing the GPS trajectory. For details on CORS, see Bruton et al (2001).



Figure 4: Lakeland Flight Trajectory

Figure 5: GPS-Estimated Exposure Station Positioning Accuracy



Figure 6: ISAT Footprint Viewer Showing Tie/Pass/GCP points for the Lakeland Flight

The exterior orientation parameters were computed in POSPAC using the terrestrially calibrated boresight. The imagery was run through ImageView for radiometric calibration. Then, the imagery, the POS-derived exterior orientation parameters, and the GCPs were introduced to Image Station for tie point collection. Figure 6 shows the layout of the entire image block including the generated tie/pass points and the GCPs. The ISAT-generated image coordinates along with the POS-generated exterior orientation data were then imported into POSCalTM. The boresight was then re-calibrated to refine the approximate boresight that was calibrated using the terrestrial calibration. Furthermore, the camera calibration parameters were checked as a quality control measure. Figure 7 shows the

image coordinate residuals for the entire block where the RMS was about 5 μ m. This is almost $\frac{1}{2}$ of the DSS imager pixel size. Figure 8 shows the refined exterior orientation and their residuals.



Figure 7: POSCalTM Showing Image Coordinate Residuals after Boresight/Camera Calibration and Q/C

POSCAL Data Explorer										_	IJ×
Block	PhotoID	X (m)	Y (m)	Z (m)	RX (m)	RY (m)	RZ (m)	W (deg)	P (deg)	K (deg)	
	1_7850_mod	408269.865	3091247.497	1909.363	0.014	0.020	-0.005	-3.241	0.834	-2.876	
🗐 🗐 Strip 2	1_7857_mod	408274.525	3091742.783	1906.929	0.007	0.025	0.070	-2.877	0.997	-3.244	
E Strip 3	1_7863_mod	408282.034	3092241.713	1905.989	0.010	0.003	0.028	-2.757	0.306	-3.544	
Strip 4	1_7870_mod	408287.007	3092740.231	1905.248	-0.026	-0.013	-0.020	-2.800	0.498	-2.754	
	1_7877_mod	408290.266	3093235.083	1903.133	-0.005	0.010	0.032	-2.906	1.329	-3.358	
Et Strip 5	1_7883_mod	408296.836	3093731.040	1901.111	-0.011	0.018	0.041	-2.746	0.682	-3.296	
III Strip 6	1_7890_mod	408301.174	3094245.227	1899.031	-0.022	0.019	0.021	-2.552	0.091	-2.367	
Project	1_7897_mod	408299.031	3094733.537	1902.794	-0.013	-0.010	0.015	-1.797	2.068	-2.939	
	1_7904_mod	408301.232	3095244.098	1905.603	-0.022	-0.012	-0.012	-2.323	1.084	-3.705	
	1_7911_mod	408306.342	3095731.293	1905.323	-0.009	-0.009	-0.018	-2.252	1.358	-4.036	
	2_8074_mod	409249.202	3095827.109	1912.424	-0.000	-0.013	-0.025	2.687	-0.674	-176.018	
	2_8083_mod	409246.645	3095328.413	1911.068	-0.011	0.002	0.015	2.891	-0.669	-176.322	
	2_8091_mod	409240.392	3094825.298	1908.731	0.003	0.001	-0.048	3.103	-1.750	-177.511	
	2_8099_mod	409231.508	3094326.314	1904.517	-0.016	-0.012	0.001	3.073	-0.877	-174.747	_
	2_8108_mod	409236.096	3093831.588	1902.651	-0.007	-0.014	-0.005	2.375	-1.889	-175.699	
	2_8116_mod	409234.454	3093334.301	1907.647	0.001	-0.004	-0.030	2.101	-1.183	-176.812	
	2_8125_mod	409230.599	3092823.687	1910.228	-0.005	-0.003	-0.042	2.311	-0.995	-176.479	
	2_8133_mod	409223.792	3092329.252	1908.868	-0.003	-0.005	-0.059	2.788	-1.608	-177.785	
	2_8141_mod	409216.573	3091830.661	1906.974	-0.009	-0.014	-0.003	2.737	-1.378	-176.888	
	2_8150_mod	409215.714	3091331.686	1907.478	-0.005	0.011	-0.045	2.140	-0.902	-176.533	
	2_8158_mod	409209.271	3090831.068	1913.884	0.024	0.012	0.037	2.521	-1.849	-178.302	
	3_8305_mod	410131.714	3090729.166	1908.460	0.004	-0.001	0.023	-2.137	1.521	-3.071	
	3_8312_mod	410145.839	3091233.087	1912.011	-0.008	-0.003	0.007	-1.608	0.137	-4.327	
	3_8319_mod	410159.291	3091725.836	1918.293	-0.007	0.005	0.040	-2.488	-0.357	-1.805	
	3_8326_mod	410161.217	3092235.278	1916.269	-0.000	-0.005	0.059	-2.931	-0.007	-1.039	
	3 8333 mod	410155.161	3092731.076	1916.578	0.022	-0.005	0.028	-2.419	1.454	-0.939	
	3_8340_mod	410151.397	3093227.315	1917.083	0.006	-0.018	-0.028	-2.888	1.598	-2.479	
	3_8347_mod	410153.982	3093730.432	1914.387	0.008	-0.000	-0.005	-2.486	0.930	-2.826	
	3 8354 mod	410160.627	3094220.190	1910.087	0.012	0.013	0.049	-3.310	2.073	-3.747	
	3 8361 mod	410175.874	3094722.664	1907.342	-0.011	-0.002	-0.003	-2.740	1.143	-4.283	-
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		1	1				-				
	Data Gra	phics Close									
P											

Figure 8: POSCalTM Showing Exterior Orientation Residuals after Boresight/Camera Calibration and Q/C

After performing the in-flight calibration and QC, the data were imported again into ISAT where the EO Analysis function (Madani and Mostafa, 2001) was used to double check the validity of the POSCalTM-calibrated parameters and to analyse the performance of the DSS. Figure 9 shows the resulted analysis. Note that the bottom panel in Figure 9 shows the statistics of the remaining y-parallax for all checkpoints showing in all possible image stereopairs, and the checkpoint residual summary. The upper edit field shows that the 'EO to Use' was chosen to be given. This implies that the exterior orientation parameters used in the EO Analysis function was the one computed by POSEO/POSCal. The second last quality control step was to run ISAT photo triangulation function using the aforementioned data. Figure 10 shows the summary of the results. After triangulating the already calibrated block of images, The EO Analysis function was run once more as the last QC step. The results of the last EO Analysis are shown in Figure 11. Note that the results shown in Figure 9 resulted from using the calibrated parameters by POSCalTM and those shown in Figure 11 resulted after running ISAT Photo triangulation on the data. Therefore, the 'EO to Use' was chosen as 'Given' in Figure 9, while chosen as 'Computed' in Figure 11. Running Photo Triangulation resulted in improving the checkpoint residuals by about 30%.

Since the GSD is 0.3 m, the resulting RMS of checkpoint residuals proved to be sub-pixel in the horizontal components. In the height component, however, the accuracy is about 2.5 pixels, which is due to the poorer geometry in the case of the DSS than that of a standard 9"x9" camera equipped with a 6" lens.

🗃, EO Analysis	;							
			E	D to Use: Given	–			
Intersected Poir	nt Results (64 Poir	its):	_					
Point Id	Type Clas	Photo Pair		Point Py (um)	Model Py (um)	DeltaX	Delta Y	Delta Z 🔺
21	Control XY2	5~5 8782 mod+5~	5 8789 mod	4.3	3.7	-0.257	0.224	0.237
21	Control XYZ	5~5 8775 mod+5~	5 8782 mod	2.3	2.3	-0.108	0.209	-0.836
22	Control XYZ	5~5 8789 mod+5~	5 8796 mod	11.4	9.9	-0.162	-0.083	0.907
22	Control XYZ	5~5 8782 mod+5~	5 8789 mod	2.9	3.7	-0.152	-0.064	-0.435
23	Control XY2	2~3~3_8361_mod+3~	3_8367_mod	1.5	2.0	-0.360	0.053	1.199
23	Control XY2	2~2_8083_mod+2~	2_8091_mod	1.3	2.1	-0.255	0.145	1.693
23	Control XY2	2~2_8091_mod+2~	2_8099_mod	2.5	2.4	-0.180	0.215	0.920
24	Control XY2	2 3~3_8340_mod+3~	3_8347_mod	2.4	4.7	0.009	0.167	1.284
24	Control XY2	2 3~3_8347_mod+3~	3_8354_mod	5.7	5.7	0.044	0.171	1.407
25	Control XY2	2 3~3_8340_mod+3~	3_8347_mod	5.1	4.7	-0.061	0.272	1.567
26	Control XY2	2 5~5_8782_mod+5~	5_8789_mod	0.7	3.7	-0.207	0.122	0.196
26	Control XY2	2 4~4_8611_mod+4~	4_8619_mod	4.0	4.1	-0.147	0.068	0.555
26	Control XY2	2 5~5_8789_mod+5~	5_8796_mod	8.0	9.9	-0.095	0.119	0.515 🚽
NE01	Control XY2	2 6~6_9015_mod+6~	6_9023_mod	5.9	3.6	0.167	0.346	-0.699
NE02	Control XY2	6~6_9015_mod+6~	6_9023_mod	1.3	3.6	-0.033	-0.289	-0.416
NNE1	Control XY2	2 5~5_8824_mod+5~	5_8831_mod	5.1	6.0	0.141	0.130	-0.502 🔄
NNE2	Control XV2	' 5~5 9921 mod±5~	5 9931 mod	63	0.3	0.169	0.1.42	.0 177
					1			
- Intersected P	oint Summarv Stat	istics						
			5114.5					
	Point Py (um):	Model Py (um):	DX (m):	DY (m):	D∠ (m):	:		
Min:	0.0	0.0	-0.803	-0.547	-1.871			
Max:	17.7	17.7	0.396	0.453	1.693	3		
Mean:	4.6	4.6	-0.132	0.075	0.018	3		
RMS:	5.7	5.8	0.262	0.209	0.786	3		
		Close	Graphics.	. [F	Report	Help	1	

Figure 9: ISAT EO Analysis Showing the Checkpoint Residuals (Lakeland Flight)

Parameter	X/Omega	Y/Phi	Z/Kappa	Key Statistics
RMS Control RMS Check RMS Limits Max Ground Residual Residual Limits Mean Std Dev Object RMS Photo Position RMS Photo Position Mean Std Dev Photo Position Mean Std Dev Photo Attitude	0.081 0.093 0.001 0.315 0.001 0.078 0.025 0.002 0.083 0.004	0.080 0.050 0.001 0.217 0.001 0.075 0.021 0.002 0.083 0.004	0.030 0.786 0.001 0.132 0.001 0.210 0.016 0.003 0.088 0.008	RMS Image (x, y): 3.0, 3.4 um Number of iterations: 3 Degrees of Freedom: 215 Gross Image Blunders: 0 Gross Control Blunders: 0 Image Blunders: 0 Solution outside of RMS tolerance. Solution outside of residual tolerance.
Current Count	0	ameras used	t (1).	
Control Points Used: 3 Check Points Used: 1 Photos Used: 6	3 - 5	Camera Id DSS_SN003	Lens Disto 0n	Linear Units: Meters Angular Units: Degrees Atm Befraction: Off
Image Points Used: 1	09			Earth Curvature: Off

Figure 10: ISAT Photo Triangulation Results (Lakeland Flight)

🐂 EO Analysis	5								_ 🗆 ×		
EO to Use: Computed											
Intersected Point Results (64 Points):											
Point Id	Туре	Class	Photo Pair		Point Py (um)	Model Py (um)	DeltaX	Delta Y	Delta Z 🔺		
23	Control	XYZ	2~2_8091_mod+2~	2_8099_mod	1.5	2.0	-0.015	0.043	0.810		
23	Control	XYZ	2~2_8083_mod+2~	2_8091_mod	6.9	7.7	-0.143	0.000	1.283		
24	Control	XYZ	3~3_8347_mod+3~	'3_8354_mod	2.7	2.7	0.098	0.090	0.381		
24	Control	XYZ	3~3_8340_mod+3~	'3_8347_mod	3.1	5.4	-0.011	0.107	0.840		
25	Control	XYZ	3~3_8340_mod+3~	'3_8347_mod	5.8	5.4	-0.089	0.153	1.160		
26	Control	XYZ	5~5_8789_mod+5~	'5_8796_mod	9.0	10.7	-0.046	0.065	0.042		
26	Control	XYZ	5~5_8782_mod+5~	5_8789_mod	1.3	3.3	-0.012	0.063	0.190		
26	Control	XYZ	4~4_8611_mod+4~	'4_8619_mod	2.6	3.2	0.131	0.145	0.122		
NE01	Control	XYZ	6~6_9015_mod+6~	'6_9023_mod	7.5	5.2	0.083	0.305	-0.270		
NE02	Control	XYZ	6~6_9015_mod+6~	'6_9023_mod	2.8	5.2	-0.047	-0.310	-0.017 🧮		
NNE1	Control	XYZ	5~5_8824_mod+5~	5_8831_mod	5.3	6.4	0.060	0.056	-0.213		
NNE2	Control	XYZ	5~5_8824_mod+5~	'5_8831_mod	7.4	6.4	0.056	0.107	0.166 🖵		
KUKIS-24	Control	~~	0~0.0001	n 0007	24	1 11	0.000	0.047	0.000		
						1					
- Intersected Pr	oint Summary	Statist	ics								
	Doint Du ().	Madal Pu (um):	DV (m)	DM (m):	DZ (m):					
	Polnicry (umj.	Model Fy (um).	DA (III).	DT (III).	UZ (III).					
Min:		0.4	0.4	-0.567	-0.468	-1.333					
Max:		13.7	13.7	0.336	0.354	1.283					
Mean:		4.4	4.4	-0.054	0.022	0.012					
RMS:		5.5	5.4	0.173	0.171	0.558					
			Class	Creation		D	l l ala	1			
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Figure 11: ISAT EO Analysis after Photo Triangulation

5. CALIBRATION VALIDATION USING THE DSS IN-FLIGHT DATA

In order to check the necessary flight data to be used to do a proper in-flight calibration and quality control (QC), the following analysis has been carried out where the effect of the number of strips and number of GCPs on boresight and camera calibration has been studied.

Simultaneously, boresight and camera calibration were computed using only 2 strips of the Lakeland flight data. All 2-strip blocks have been used several times to account for the effect of the number of ground control points. The resulting boresight angles and principal point offsets were compared to the reference calibration parameters which were computed using the entire block of images. The differences are assumed here to be the accuracy of the calibration of boresight and principal point offsets. Figure 12 and Figure 13 show the accuracy of boresight and camera calibration using 2 strips of images for different. Note the strong correlation between the principal point offset in x and y components and the boresight angles in the same direction (i.e., around the x and y axis). The same analysis has been done for 3-strip blocks and 4-strip blocks. Figure 14 and Figure 15 show the same results for a 3-strip block of images, while Figure 16 and Figure 17 show the results for 4-strip block of images.



Figure 12 Boresight Difference Using 2 Image Strips



Figure 14: Boresight Difference Using 3 Strips



Figure 16: Boresight Difference Using 4 Strips



Figure 13: Principal Point Offset Difference Using 2 Strips



Figure 15: Principal Points Offset Difference Using 3 Strips



Figure 17: Principal Point Offset Difference Using 4 Strips

It is clear from the analysis presented in Figures 12, 13, 14, 15, 16, and 17, that the boresight and principal point offset calibration using flight data is very stable and consistent when using different GCPs and even without using any GCPs. This is one of the design elements of POSCal^{TM,} which is boresight and camera calibration to be done without the need for ground control (see Mostafa, 2001). However, when using only 2 strips of images, the boresight/camera calibration was not consistent when using different 2-strip blocks. That is, for example, the boresight and principal point offsets computed using strips number 1 and 2 are different from those computed using strip number 2 and 3, respectively. On the other hand, boresight and principal point offset calibration was very stable and consistent when using different 3-strip and 4-strip blocks. Therefore, it is recommended to use at least 3 strips of images of at least 8 images each to calibrate the boresight and camera parameters.

6. CONCLUSIONS

Emerge Digital Sensor System (DSS) has been designed for orthophoto generation data collection. It consists of a 4kx4k digital camera, a POS AV system, and a flight management system. The DSS has been tested in numerous test flights since the Spring of 2002. The test results and analysis of one of the flights that was flown over a test field in Lakeland, Florida, are presented. The results proved that the DSS different components and the system as a whole performed to the system specifications. When flying the DSS equipped with a 55 m lens over Lakeland from a 2000 m flight altitude (which resulted in a 0.3 m ground sample distance) the accuracy of directly computing the coordinates of GCPs were at 0.2 and 0.25 m accuracy in X, and Y respectively and 0.8 m in the elevation. Running the entire data set through Photo-T showed an accuracy improvement of about 30% in all three coordinate components. To study the accuracy of calibration using the necessary number of images and image strips, a number of simultaneous boresight/ camera calibration were done using 2-strip, 3-strip, and 4-strip image blocks. The results show that the 2-strip image block is not consistent enough to do the calibration. However, for the 3-strip and 4-strip blocks the results are very stable and consistent when using different configurations of 3- and 4-strip blocks and different configuration of GCPs. It is therefore, recommended to use the data processing flow described in this article and following the quality control procedure presented here when processing DSS-derived data.

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